

**Amendments to the Drawings:**

The attached six (6) sheets of drawings include changes to Figs. 1, 1a, 2, 2a, 3, 4, 4a, and 5. The attached replacement sheets, which include Figs. 1, 1a, 2, 2a, 3, 4, 4a, and 5, replace the original sheet including Figs. 1, 1a, 2, 2a, 3, 4, 4a, and 5. In Figs. 1, 1a, 2, 2a, 3, 4, 4a, and 5, descriptive legends for the boxes have been provide.

### Remarks

This Preliminary Amendment cancels without prejudice original PCT claims 1-44 in the underlying PCT Application No. PCT/DE02/04546, as well as canceling substitute claims 1-32 presented in the Preliminary Examination Report, and adds new claims 45-76. The new claims conform to U.S. Patent and Trademark Office rules and do not add new matter to the application.

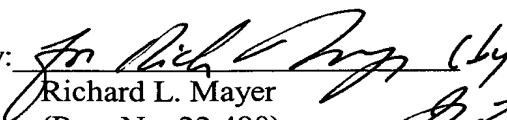
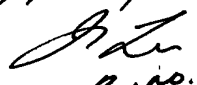
In accordance with 37 C.F.R. § 1.125(b), the Substitute Specification (including the Abstract, but without the claims) contains no new matter. The amendments reflected in the Substitute Specification (including Abstract) are to conform the Specification and Abstract to U.S. Patent and Trademark Office rules or to correct informalities. As required by 37 C.F.R. § 1.121(b)(3)(ii) and § 1.125(c), a Marked Up Version Of The Substitute Specification comparing the Specification of record and the Substitute Specification also accompanies this Preliminary Amendment. Approval and entry of the Substitute Specification (including Abstract) are respectfully requested.

The underlying PCT Application No. PCT/DE02/04546 includes an International Search Report, dated April 9, 2003. The Search Report includes a list of documents that were uncovered in the underlying PCT Application. A copy of the Search Report accompanies this Preliminary Amendment. Also enclosed is an English translation of the International Preliminary Examination Report dated March 12, 2004.

Applicants assert that the subject matter of the present application is new, non-obvious, and useful. Prompt consideration and allowance of the application are respectfully requested.

Respectfully Submitted,  
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METHOD FOR OPERATING AN INTERNAL COMBUSTION ENGINE

Related Art FIELD OF THE INVENTION

The present invention relates to a control unit and a method for operating an internal combustion engine of a motor vehicle, ~~in particular, having a control device for~~ controlling/regulating such that the internal combustion engine is controlled/regulated as a function of an air-mass sensor signal ~~from a first air-mass sensor~~.

~~Furthermore, the present invention relates to an internal combustion engine of a motor vehicle, in particular, having a control unit for controlling/regulating the internal combustion engine as a function of an air-mass sensor signal from a first air-mass sensor.~~

~~The present invention also relates to a control unit for an internal combustion engine of a motor vehicle, in particular, for controlling/regulating the internal combustion engine as a function of an air-mass sensor signal from a first air-mass sensor.~~

BACKGROUND INFORMATION

If a fault occurs in the air-mass sensor signal of the air-mass sensor ~~itself~~, known operating methods have the disadvantage that the control/regulation of the internal combustion engine is influenced in such a way that the internal combustion engine will no longer ~~be working in~~ operate at the optimal operating point.

When driving on a wet surface, for instance, spray water may get into an intake tract of the internal combustion engine, where it can penetrate an air filter and wet an air-mass sensor installed in the intake tract. This effect, which is also known as water entry, is particularly disadvantageous ~~in~~ for the widely used hot-film air-mass sensors, which have a heating surface that cools ~~spontaneously~~ when ~~coming~~ brought into contact with water in the liquid phase, with the result that the air-mass sensor signal generated by the air-mass sensor is ~~falsified~~ distorted.

Using the ~~falsified~~ distorted air-mass sensor signal, the control unit controlling/regulating the internal combustion engine calculates an incorrect value for the air-fuel ratio to be set, so that the internal combustion engine ~~is~~ no longer ~~working in~~ operates at the optimal operating point, ~~as mentioned earlier~~.

Furthermore, the emission values of the internal combustion engine are affected by water entry, since a portion of the introduced water or the water vapor generated therefrom reaches a combustion chamber of the internal combustion engine, where it displaces a portion of the air quantity required for combustion.

#### ~~Advantages of the Invention~~

Accordingly, it is ~~the~~ an object of the present invention to provide a method for operating an internal combustion engine that minimizes ~~especially~~ the influence of an interference variable, which affects the air-mass sensor signal, ~~on~~ and in turn effects the regulation of the internal combustion engine.

#### SUMMARY

~~In a method of the type mentioned in the introduction~~

~~accordance with the present invention, this objective is~~  
~~attained in that~~ at least one first auxiliary signal is  
utilized, and ~~that~~ the influence of an interference variable,  
which affects the air-mass sensor signal, ~~on and in turn~~  
5 ~~effects~~ the regulation of the internal combustion engine, is  
reduced as a function of the first auxiliary signal.

The inclusion of the first auxiliary signal according to the  
present invention makes it possible for the internal  
10 combustion engine to ~~work in~~ operate at the optimal operating  
point despite a fault in the air-mass sensor signal. Compared  
to conventional operating methods for internal combustion  
engines, an optimal power output of the internal combustion  
engine is ensured even when driving on wet surfaces, and  
15 compliance with legally mandated limit values for emissions of  
the internal combustion engine is ~~given~~ ensured as well.

An advantageous ~~specific~~ example embodiment of the operating  
method according to the present invention ~~is characterized in~~  
20 ~~that~~ includes a comparison of the first auxiliary signal, or  
~~of~~ a signal derived from the first auxiliary signal, with the  
air-mass sensor signal, or a signal derived from the air-mass  
sensor signal, ~~is performed~~ and a comparison result is  
obtained.

25 Comparing the first auxiliary signal with the air-mass sensor  
signal makes it possible to ~~conclude~~ determine a fault of the  
air-mass sensor in the case of substantially different signal  
characteristics. In this manner, wetting of the heating  
30 surface of a hot-film air-mass sensor with water, for  
instance, is able to be detected. It is also possible to  
detect other types of faults of the air-mass sensor, for  
instance a signal cut-off of the sensor caused by mechanical  
damage to a signal line.

35 A direct comparison of a signal derived from the first

auxiliary signal with the air-mass sensor signal or ~~also~~ with  
a signal derived from the air-mass sensor signal is  
particularly advantageous. This makes it possible to include  
only certain signal components of the first auxiliary signal  
in the comparison.

Another ~~specific example~~ embodiment of the operating method  
according to the present invention ~~is characterized in that~~  
includes obtaining a controlled variable for the control of  
the internal combustion engine ~~is obtained~~ as a function of  
the comparison result. The use of this controlled variable  
allows the control/regulation of the internal combustion  
engine to be adapted in such a way that a compensation of the  
influence of the disturbance variable on the air-mass sensor  
signal may take place.

In a ~~very simple~~ variant of the method, the controlled  
variable may be obtained from the difference of a first  
auxiliary variable, interpreted as setpoint value for the air  
mass flowing into the intake tract, and the air-mass sensor  
signal.

In a further ~~development~~ variant of this method ~~variant~~, it is  
additionally possible to obtain the controlled variable from  
the first auxiliary signal alone; this is ~~always~~ useful when  
the air-mass sensor signal deviates significantly from an  
expected value. When the air-mass sensor is not available at  
all, the method according to the present invention will still  
allow the internal combustion engine to be operated ~~in~~ at the  
optimal operating point.

Another advantageous ~~specific example~~ embodiment of the  
operating method according to the present invention ~~is~~  
~~characterized by~~ includes obtaining the first auxiliary signal  
~~being obtained~~ from state variables of the internal combustion  
engine, so that no additional external sensors are necessary

to obtain the first auxiliary signal. Instead, the first auxiliary signal may be ascertained from the position of a driver pedal, the rotational speed, the temperature, as well as other state variables of the internal combustion engine.

5 Another, ~~especially~~ advantageous ~~specific~~ example embodiment of the present invention ~~is characterized by~~ includes obtaining the first auxiliary signal ~~being obtained~~ from a signal of an exhaust-gas probe such as a lambda probe. In this  
10 ~~specific~~ embodiment, it is possible to subject the air-mass sensor signal to a plausibility check since, with knowledge of the injected fuel quantity, the fuel mass actually conveyed to the combustion chamber may be calculated from the signal of the exhaust-gas probe. In contrast to the air-mass sensor  
15 signal, the signal of the exhaust-gas analyzer probe is not greatly ~~falsified~~ distorted by the water vapor in the combustion chamber.

If the first auxiliary signal deviates significantly from the  
20 air-mass value obtained from the air-mass sensor signal, a malfunction of the first air-mass sensor may be concluded, possibly due to water in the intake tract. In this case, the operating method according to the present invention ~~even~~ makes it possible to, e.g., discard the faulty air-mass sensor  
25 signal and ~~to~~ substitute the first auxiliary signal as input variable for the control device of the internal combustion engine.

To consider the generally higher dynamics of a hot-film  
30 air-mass sensor compared to a lambda probe, the measured values of the air-mass sensor signal may be averaged. As an alternative, it is possible to connect a filter downstream from the air-mass sensor, which describes the dynamics of the controlled system of the lambda probe. If the internal  
35 combustion engine is a diesel gasoline engine, a lean-mixture sensor may be used as exhaust-gas probe.

~~It is preferred if a~~ A permanent comparison of the air-mass sensor signal with the signal from the exhaust-gas probe ~~takes~~ may take place within the framework of the afore-described plausibility control of the air-mass sensor signal, the controlled variable for regulating/controlling the internal combustion engine being obtained as a function of the comparison result.

~~Another~~ In accordance with advantageous ~~specific example~~ embodiment of the operating method according to the present invention, ~~is characterized by~~ the comparison ~~including~~ includes the following steps: differentiating the air-mass sensor signal so as to obtain a differentiated air-mass sensor signal; differentiating the first auxiliary signal to obtain a differentiated auxiliary signal; and forming the difference from the differentiated air-mass sensor signal and the differentiated auxiliary signal to obtain a differential signal, the differential signal being a measure for the difference in the time change between the signal from the first air-mass sensor and the first auxiliary signal. The first auxiliary signal ~~is preferably~~ may be obtained from the state variables of the internal combustion engine or from the signal of an exhaust-gas probe and may be interpreted as setpoint value for the air mass.

If the differential signal exceeds a predefinable threshold value, which corresponds to a dynamic response of the air-mass sensor signal that deviates significantly from the first auxiliary signal, a malfunction or a fault of the air-mass sensor is detected in this ~~specific example~~ embodiment. It is advantageous for simple processing of the differential signal if the differentiated air-mass sensor signal is scaled to a time average of the air-mass sensor signal, the differentiated auxiliary signal is scaled to a time average of the first auxiliary signal, and the absolute value of the differential signal is generated so as to obtain a positive differential



signal. Finally, the differential signal is compared to at least one predefinable threshold value. If the afore-mentioned absolute-value generation is omitted, two threshold values for the differential signal must be selected accordingly.

5 The threshold value makes it possible to specify the maximum value[[/]] or the extremal values of the differential signal at which a difference between the air-mass sensor signal and the first auxiliary signal is not yet interpreted as fault of  
10 the air-mass sensor signal.

In the case of a single threshold value and in the event that it is exceeded, the first auxiliary signal is obtained as controlled variable. The air-mass sensor signal is obtained as  
15 controlled variable if the comparison result indicates that the differential signal is smaller than or equal to the threshold value. An analogous procedure is proposed in the case of two threshold values.

20 In a further advantageous ~~specific~~ example embodiment of the operating method according to the present invention, the first auxiliary signal is obtained from a signal of a second air-mass sensor. The additional, second air-mass sensor, just like the exhaust-gas probe, allows a plausibility control of  
25 the air-mass sensor signal from the first air-mass sensor.

Another advantageous ~~specific~~ example embodiment of the present invention provides that the first auxiliary signal be obtained from a signal of an already present rain sensor of  
30 the motor vehicle. Rain sensors are used to control windshield wipers, for example, and the signals they provide may be utilized as a measure for the precipitation quantity. From the precipitation quantity, which is correlated to the interference variable influencing the air-mass sensor signal,  
35 namely the water quantity striking the heating surface of the hot-film air-mass sensor, the controlled variable may be

ascertained.

Another ~~advantageous specific example~~ embodiment of the present invention ~~is characterized in~~ provides that the first auxiliary signal is obtained from a signal of a capacitive sensor, the capacitive sensor being configured as integral component of the first air-mass sensor. A variant having an especially small design results from the fact that the surface of the already present first air-mass sensor is used as first capacitor plate of the capacitive sensor. A second capacitor plate of the capacitive sensor may be arranged in a housing of the first air-mass sensor, for example.

Another advantageous ~~specific example~~ embodiment of the present invention ~~is characterized in~~ provides that the first auxiliary signal is obtained from a signal of an ohmic sensor, the ohmic sensor being configured as integral component of the first air-mass sensor. An ~~especially advantageous specific example~~ embodiment of the method according to the present invention ~~is characterized by~~ provides that the ohmic sensor ~~having~~ has at least two electrodes preferably made of a corrosion-resistant material. This ensures that the ohmic sensor is also suited for long-term operation.

A ~~very advantageous further specific example~~ embodiment of the present invention provides for the ohmic sensor to be arranged on the surface of the first air-mass sensor.

In an advantageous further ~~development~~ embodiment of the operating method according to the present invention, the first auxiliary signal is obtained from the signal of the capacitive sensor and the signal of the ohmic sensor. Water droplets striking the surface of the air-mass sensor are able to be detected in a reliable manner by changes in the capacitance or the conductivity of the respective sensor. If a hot-film air-mass sensor is used, an arrangement of the

capacitive/ohmic sensor directly on the heating surface ~~is~~  
~~useful~~ may be used.

Within the framework of the comparison, an ~~especially~~  
5 advantageous ~~specific~~ example embodiment of the method  
according to the present invention provides for a difference  
to be formed from the first auxiliary signal and the air-mass  
sensor signal so as to obtain the controlled variable. The  
first auxiliary signal ~~is preferably~~ may be determined from  
10 the state variables of the internal combustion engine, such as  
the driver-pedal position, the rotational speed and additional  
variables. The first auxiliary signal in this case represents  
a setpoint value for the air mass to be ~~conducted~~ conveyed to  
the internal combustion engine, the setpoint value being  
15 obtained from the state variables of the internal combustion  
engine. This allows a comparison with the air-mass signal  
actually detected by the air-mass sensor.

A filtering of the air-mass sensor signal prior to forming the  
20 difference is ~~particularly~~ advantageous for obtaining a  
filtered air-mass sensor signal. In this way, only the signal  
frequencies of the air-mass sensor signal that are meaningful  
for the comparison are considered in the comparison. For  
example, when a low pass filter is used for filtering, high  
25 frequency signal components of the air-mass sensor signal are  
filtered out and will not be entered in the difference  
generation.

~~From measurements it~~ It is known that such high frequency  
30 signal components of the air-mass sensor signal are produced  
by water droplets hitting the heating surface of the air-mass  
sensor and by the related spontaneous cooling of the heating  
surface.

35 These high frequency signal components may be considered an  
interference variable since they do not contain any directly

analyzable information about the air mass entering via the intake tract and have an interfering effect on the difference formation and thus on the controlled variable as well. This is prevented by using a low pass filter according to the present invention. It is ~~particularly~~ useful in this context to select the cut-off frequency of the low pass filter such that the low pass filter filters out the highest possible portion of the signal energy of the high frequency signal components so as to minimize the influence of the interference variable.

To this end, an ~~especially advantageous variant~~ example embodiment of the method according to the present invention provides that the cut-off frequency of the low pass filter be selected dynamically and as a function of state variables of the internal combustion engine. This allows an especially good suppression of the interference variable via the low pass filter. Furthermore, additional interfering signal components of the air-mass sensor signal whose spectrum depends on the operating state of the internal combustion engine may be suppressed in this manner.

~~A highly advantageous~~ An additional specific example embodiment of the operating method according to the present invention ~~is characterized in~~ provides that the cut-off frequency of the low pass filter is selected as a function of a model of the internal combustion engine. A so-called system model of the internal combustion engine may be used as model, which provides information regarding the spectrum of allowed air-mass sensor signals in the respective state of the internal combustion engine as a function of the state variables of the internal combustion engine.

Using this information, the cut-off frequency of the low pass filter is able to be selected in such a way that only spectral components of the air-mass sensor signal that are not caused by an interference effect are entered in the difference

formation.

A further ~~specific example~~ embodiment of the method according to the present invention ~~is characterized in~~ provides that the first auxiliary signal is obtained from the air-mass sensor signal by filtering with a high pass filter and is used as a controlled variable to control the internal combustion engine.

As already mentioned, it is known that water droplets striking the heating surface of a hot-film air-mass sensor cause high frequency signal components, ~~in particular,~~ which are able to be separated from the low frequency signal components of the air-mass sensor signal by the high pass filter utilized according to the present invention. In this case the first auxiliary signal is a measure for the water quantity striking the air-mass sensor and may be used as controlled variable.

In this ~~variant embodiment~~ as well, the selection of the cut-off frequency of the high pass ~~must be~~ is implemented dynamically and as a function of state variables of the internal combustion engine in order to increase the accuracy of the method, thereby preventing the possibility that the first auxiliary signal also contains signal components of a useful signal of the air-mass sensor.

Another ~~specific example~~ embodiment of the method according to the present invention ~~is characterized by~~ provides a second auxiliary signal being obtained from the air-mass sensor signal via filtering with a low pass filter, and ~~by~~ the controlled variable being obtained from the first auxiliary signal, the second auxiliary signal and state variables of the internal combustion engine. In this ~~specific example~~ embodiment, the first auxiliary signal constitutes a measure for the water quantity striking the air-mass sensor; the second auxiliary signal constitutes the actual useful signal of the air-mass sensor representing the air mass flowing

through the intake tract; and from the state variables of the internal combustion engine it is possible in turn to dynamically select a cut-off frequency of the low pass/high pass filter.

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It is conceivable that the cut-off frequency of the low pass filter corresponds to the cut-off frequency of the high pass filter. To obtain a spectral separation of the first and the second auxiliary signal, a band stop may be utilized instead of the low pass filter and the high pass filter, the band stop's lower cut-off frequency matching the cut-off frequency of the low pass filter and its upper cut-off frequency matching the cut-off frequency of the high pass filter.

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According to a further advantageous ~~specific~~ example embodiment of the present invention, the cut-off frequency of the high pass/low pass filter is selected as a function of a model of the internal combustion engine. As an alternative, it is also possible for the upper and the lower cut-off frequency of the band stop to be selected as a function of a model of the internal combustion engine.

20

Another, ~~especially~~ advantageous ~~specific~~ example embodiment of the ~~method according to the~~ present invention ~~in which~~ provides two air-mass sensors ~~are~~ arranged in an intake manifold of the internal combustion engine in such a way that air flowing into the intake manifold first reaches the first air-mass sensor and then the second air-mass sensor, which is located at a distance in the flow direction of the aspirated air, and the method includes the following steps within the framework of the comparison: ~~Delaying~~ delaying the air-mass sensor signal by a delay time so as to obtain a delayed air-mass sensor signal; subtracting the first auxiliary signal from the delayed air-mass sensor signal in order to obtain a differential signal; integrating the differential signal so as to obtain an indicator signal; differentiating the delayed

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air-mass sensor signal to obtain a differentiated air-mass sensor signal; forming the amount of the differentiated air-mass sensor signal to obtain a positive air-mass sensor signal; differentiating the first auxiliary signal to obtain a differentiated auxiliary signal; forming the amount of the differentiated auxiliary signal to obtain a positive auxiliary signal; and subtracting the positive auxiliary signal from the positive air-mass sensor signal to obtain an additional differentiated signal.

The indicator signal obtained from the differentiated signal is a measure for the water quantity present in the intake manifold or in the intake tract; ~~and~~ the operational sign of the additional differentiated signal indicates which one of the two air-mass sensors provides the greater signal change. According to the present invention, when a predefinable threshold value for the indicator signal is exceeded, i.e., in the case of water entry into the intake tract, the controlled variable is obtained from the indicator signal and the signal of the particular air-mass sensor for which the smaller signal change has been detected. This mechanism takes the fact into account that high-frequency signal components in the air-mass sensor signal are in all likelihood caused by water droplets striking the heating surface of an air-mass sensor, or originate from other interference effects and not from usually low-frequency changes in the air-mass flow through the intake tract that are appropriate to the operation.

Another advantageous ~~specific~~ example embodiment of the method according to the present invention ~~is characterized in~~ provides that both air-mass sensors are arranged next to one another, ~~in~~ that the delay step is omitted, ~~and in~~ that the second air-mass sensor is provided with a water-droplet separator. In another example method ~~variant~~ according to the present invention, it is ~~especially~~ advantageous that a model simulating the dynamic response of the water-droplet separator

is taken into account in the processing of the air-mass sensor signal and/or the first auxiliary signal. The model makes it possible to consider the dynamic response of the second air-mass sensor, which is changed because of the water-droplet separator, thereby ensuring the comparability of the sensor signals from the first air-mass sensor and the second air-mass sensor.

Another ~~specific example~~ embodiment of the method according to the present invention ~~is characterized by~~ provides both air-mass sensors being integrated in a shared sensor system, preferably e.g., in a shared housing.

Another, ~~especially~~ advantageous ~~specific example~~ embodiment of the method according to the present invention ~~is characterized in~~ provides that the first air-mass sensor is designed as hot-film air-mass sensor.

~~Of special importance is the~~ The implementation of the method according to the present invention may be in the form of a computer program which is provided for a control unit of an internal combustion engine in a motor vehicle, ~~in particular.~~ The computer program has program codes suitable for carrying out the method according to the present invention when it is executed on a computer. Furthermore, the program code may be stored on a computer-readable data carrier, such as ~~in a~~ so-called flash memory. In these cases, the present invention is thus realized by the computer program, ~~so that the computer program represents the present invention in the same manner as the method for whose execution the program is suitable.~~ ~~As an additional attainment of the object of the present invention, an internal combustion engine is indicated as recited in Claim 43. Still another attainment of the object of the present invention is given by a control unit as recited in Claim 44.~~



~~Further features, uses and advantages of the present invention come to light from the following description of exemplary embodiments of the present invention, which are shown in the figures of the drawing. In this context, all of the described or represented features, by themselves or in any combination, form the subject matter of the present invention, regardless of their combination in the patent claims or their antecedents, and regardless of their formulation and representation in the specification and drawing, respectively.~~

~~The figures show:~~ BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic illustration of signal flow ~~chart on which according to a first specific example~~ embodiment of the method according to the present invention ~~is based,~~

Figure 1a is a flow chart corresponding to the signal flow ~~chart of shown in~~ Figure 1[[]].

Figure 2 is a schematic illustration of signal flow ~~chart of according to a second specific example~~ embodiment of the present invention[[]].

Figure 2a is a flow chart corresponding to the signal flow ~~chart of shown in~~ Figure 2[[]].

Figure 3 is a schematic illustration of signal flow ~~chart of according to a third specific example~~ embodiment of the method according to the present invention[[]].

Figure 4 is a schematic illustration of the arrangement of the hot-film air-mass sensors HFM\_1, HFM\_2 in intake manifold 4 ~~in a schematic representation, as well as the associated signal flow chart,~~

Figure 4a is a flow chart of the third specific example

embodiment of the method according to the present invention,  
and.

Figure 5 shows a schematic illustration of an internal  
combustion engine according to the present invention.

#### DETAILED DESCRIPTION

Figure 1 shows a signal flow ~~chart~~ of a first example method  
~~variant~~ according to the present invention, in which a first  
auxiliary signal H\_1 ~~together with~~ and an air-mass sensor  
signal L\_1 from a first hot-film air-mass sensor HFM\_1 (Figure  
5) ~~is~~ are analyzed. Air-mass sensor HFM\_1 is arranged in  
intake tract 3 of an internal combustion engine 1 (Figure 5),  
and emits a signal L\_1 whose value is proportional to the air  
mass flowing through the intake tract.

The evaluation of signals L\_1, H\_1 makes it possible to reduce  
the influence of an interference variable, which affects  
air-mass sensor signal L\_1, ~~on~~ and in turn effects the  
control/regulation of internal combustion engine 1 implemented  
by control unit 2. The time sequence of the method steps for  
the evaluation may be ~~gathered~~ seen from the flow chart of  
Figure 1a.

As can be seen in Figure 1, auxiliary signal H\_1 is obtained  
from the following state variables of internal combustion  
engine 1: ~~from~~ pressure P of the fresh air outside intake  
tract 3; ~~from~~ temperature T of the fresh air; and ~~from~~ the  
rotational speed n of internal combustion engine 1; ~~as well as~~  
~~possibly from~~ additional state variables (not shown) of  
internal combustion engine 1 may also be used, as well.  
Auxiliary signal H\_1 indicates the air mass determined from  
state variables P, T, n with the aid of the general gas  
equation, the air mass being the air mass required by internal  
combustion engine 1 during the operation with state variables

P, T, n.

First auxiliary signal H<sub>1</sub> is conveyed to differentiator 20, which, in step 211 of the flow chart of Figure 1a, forms a differentiated auxiliary signal H<sub>1\_1</sub> from first auxiliary signal H<sub>1</sub>.

Next, in step 211a of Figure 1a, differentiated auxiliary signal H<sub>1\_1</sub> is scaled to a time average H<sub>1\_m</sub> of first auxiliary signal H<sub>1</sub>.

In parallel with steps 211, 211a, air-mass sensor signal L<sub>1</sub> of first air-mass sensor HFM<sub>1</sub> (Figure 5) is transmitted to a further differentiator 21 (Figure 1), which takes place in step 210 of Figure 1a. Differentiator 21 of Figure 1 delivers a differentiated air-mass sensor signal L<sub>1\_1</sub>, which, in a following step 210a (Figure 1a), is scaled to a time average L<sub>1\_m</sub> of air-mass sensor signal L<sub>1</sub>.

The difference generation from differentiated air-mass sensor signal L<sub>1\_1</sub> and differentiated auxiliary signal H<sub>1\_1</sub> in subtractor 22 (Figure 1), which follows in step 220, yields a differential signal D<sub>1\_1</sub>. Finally, in step 230, the amount of differential signal D<sub>1\_1</sub> is formed so as to obtain a positive differential signal D<sub>1\_1'</sub>, which is filtered by a filter 23 in following step 240.

Filtered differential signal D<sub>1\_1</sub>\* is compared in a comparator 24 with a predefinable threshold value S<sub>1</sub> in order to obtain a comparison result VE. The comparison of filtered differential signal D<sub>1\_1</sub>\* with predefinable threshold value S<sub>1</sub> takes place in step 250 of Figure 1a.

Two possible comparison results VE exist in comparison 250 with predefinable threshold value S<sub>1</sub> for filtered differential signal D<sub>1\_1</sub>\*, which is always positive due to

the amount generation in step 230.

Differential signal D\_1\_1 indicates the difference between the time change of air-mass sensor signal L\_1 of first air-mass sensor HFM\_1 and the time change of first auxiliary signal H\_1. For as long as differential signal D\_1\_1 does not exceed a ~~certain~~ selected limit value, it is assumed that no interference influence of signal L\_1 from air-mass sensor HFM\_1 exists. In this case, signal L\_1 is obtained as controlled variable R (Figure 1a).

However, as soon as the limit value is exceeded, it is assumed that an interference influence of signal L\_1 is present, which represents the cause of the deviating dynamic response of signals L\_1, H\_1. In this case, first auxiliary signal H\_1 is obtained as controlled variable R, i.e., control unit 2 shown in Figure 5 does not receive a signal L\_1 from an external sensor as input variable for the air flowing through intake tract 3, but a variable that is calculated in control unit 2 itself.

The interference influence may stem from interferences resulting from high-frequency electromagnetic radiation in the area of connecting lines of air-mass sensor HFM\_1. Another cause ~~is~~ may be attributable to water droplets striking the heating surface of air-mass sensor HFM\_1 and the spontaneous cooling of the heating surface that accompanies it.

The ~~described~~ method according to the present invention prevents speed fluctuations or a sudden drop in the output of internal combustion engine 1, and also the exceeding of limit values for the emissions of internal combustion engine 1[[;]]; this is due to the fact that in a malfunction of air-mass sensor signal L\_1, auxiliary signal H\_1 is substituted as controlled variable R or as input variable for control unit 2 of internal combustion engine 1.

The signal flow ~~chart~~ of a second ~~specific~~ example embodiment of the present invention is shown in Figure 2, ~~and which~~ simultaneously ~~shows~~ represents a closed-loop control circuit of internal combustion engine 1. The associated method flow chart may be ~~gathered~~ seen from Figure 2a.

As can be ~~inferred~~ seen from Figure 2, air-mass sensor HFM\_1 provides an air-mass sensor signal L\_1, which is obtained from the value of the air mass in intake tract 3 of internal combustion engine 1 and an interference variable S\_X that is superposed onto this value.

As already mentioned, interference variable S\_X ~~symbolizes~~ represents signal interferences of air-mass sensor signal L\_1, which are caused, for instance, by water droplets striking the heating surface of air-mass sensor HFM\_1.

According to Figure 2a, signal L\_1 is first filtered by a low pass filter 340a in a step 340, which results in a filtered air-mass sensor signal L\_1\*. Filtered air-mass sensor signal L\_1\* is subsequently subtracted from an auxiliary signal H\_1 in a step 380.

As in the previous example, auxiliary signal H\_1 is arithmetically obtained from state variables P, T, n of internal combustion engine 1. Difference generation 380 provides controlled variable R, which is supplied as input variable to control unit 2 and influences the regulation of internal combustion engine 1.

Controlled variable R acts on a closed-loop control circuit for the exhaust-gas recirculation, for instance. This makes it possible to adjust the air-fuel mixture conveyed to internal combustion engine 1 to an optimal value.

In the ideal state, controlled variable R assumes the value

zero, i.e., the air mass recorded by air-mass sensor HFM\_1 is as large as the arithmetically determined air mass of auxiliary signal H\_1. As soon as interference variable S\_X assumes a value other than zero, for instance when water enters the intake tract, a non-zero value results for controlled variable R as well.

To prevent ~~that the~~ interference variable S\_X ~~influences from~~ influencing the regulation of the exhaust-gas recirculation, air-mass sensor signal L\_1 is filtered by low pass filter 340a. On the basis that interference variable S\_X usually provides high-frequency signal components compared to the air mass to be measured, in particular when water has entered intake tract 3, the cut-off frequency of low pass filter 340a is selected such that ~~merely all~~ only low-frequency signal components of air-mass sensor signal L\_1 are allowed to pass and are thus considered when determining controlled variable R. High frequency signal components attributable to the interference variable will not be allowed to pass by 340a and are thus unable to influence the formation of controlled variable R.

It is ~~particularly~~ advantageous to select the cut-off frequency dynamically, i.e., during operation of internal combustion engine 1, that is to say, as a function of a so-called system model of internal combustion engine 1. The system model provides information concerning the spectrum of air-mass sensor signal L\_1 as a function of state variables P, T, n.[[, ...]] This information also includes the highest signal frequency of signal L\_1 to be expected. On the basis of this information it is possible to include in the generation of controlled variable R only that part of the spectrum of signal L\_1 that indicates the actually recorded air mass.

Figure 3 shows the signal flow ~~chart of a variant~~ according to an example embodiment of the present invention, which includes

both a high pass filter 440a and also a low pass filter 442a.

On the basis of air-mass sensor signal L\_1 of air-mass sensor HFM\_1, first auxiliary signal H\_1 is obtained from high-pass filtering of signal L\_1 using high-pass filter 440a. Second auxiliary signal H\_2 is obtained from low-pass filtering of signal L\_1 using low pass filter 442a.

Controlled variable R is obtained from the two auxiliary signals H\_1, H\_2, analogously to the previous examples, from state variables (not shown in Figure 3) of internal combustion engine 1 (cf. Figure 5).

In this ~~variant~~ embodiment, the water quantity in intake tract 3 of internal combustion engine 1 is represented by auxiliary signal H\_1, which, due to the high-pass filtering, includes only the signal components stemming from the water droplets striking the heating surface of sensor HFM\_1.

The low-frequency signal components of air-mass sensor signal L\_1, which indicate the actual air-mass flow, form second auxiliary signal H\_2.

The cut-off frequencies of filters 440a, 442a are selected as a function of a model of internal combustion engine 1 and are dynamically adapted to the individual operating state.

With knowledge of the water quantity in intake tract 3 from first auxiliary signal H\_1, the actual air mass from second auxiliary signal H\_2, and from state variables of internal combustion engine 1 (as well as possibly additional parameters of the combustion), it is possible to calculate the air mass actually available in the combustion chambers of internal combustion engine 1.

Even with water in its liquid phase present in intake tract 3

of internal combustion engine 1, it is possible to operate internal combustion engine 1 ~~in~~ at the optimal operating point.

5 Another ~~specific~~ example embodiment of the present invention is shown in Figure 4. Two hot-film air-mass sensors HFM\_1, HFM\_2 are arranged in intake manifold 4 at a clearance D with respect to one another. The arrow ~~symbolizes~~ indicates the flow direction of the air flowing into intake manifold 4.

10 As can be gathered from Figure 4, first air-mass sensor HFM\_1 is first surrounded by an inflowing air volume, and, following a propagation delay as a function of clearance D, second hot-film air-mass sensor HFM\_2 is surrounded by the inflowing  
15 air volume as well.

First sensor HFM\_1 provides air-mass sensor signal L\_1, and second sensor HFM\_2 provides first auxiliary signal H\_1. To compensate for the propagation-delay difference between  
20 air-mass sensor signal L\_1 and first auxiliary signal H\_1 caused by clearance D, timing element 510a is provided. It delays (cf. flow chart Figure 4a) air-mass sensor signal L\_1 by the time required by an air volume flowing into intake manifold 4 to travel from first sensor HFM\_1 to second sensor  
25 HFM\_2 and provides delayed air-mass sensor signal L\_1\_delta\_T, which is subsequently differentiated in differentiator 540a so as to obtain a differentiated air-mass sensor signal L\_1\_delta\_T\_1. The delay time of timing element 510a is adjustable and is selected such that the difference from  
30 signals L\_1\_delta\_T and H\_1 is zero when no water is present in intake manifold 4.

First auxiliary signal H\_1 provided by second sensor HFM\_2 is differentiated in differentiator 542a to obtain a  
35 differentiated auxiliary signal H1\_1. Both differentiators 540a, 542a also perform an amount generation, so that a



positive air-mass sensor signal L\_1\_delta\_T\_1' and a positive auxiliary signal H1\_1', respectively, ~~is~~ are present at the individual ~~output~~ outputs.

5 Finally, positive auxiliary signal H1\_1' is subtracted from positive air-mass sensor signal L\_1\_delta\_T\_1' in order to obtain a further differential signal Z\_Diff.

10 Furthermore, first auxiliary signal H\_1 is subtracted from delayed air-mass sensor signal L\_1\_delta\_T, and resulting differential signal D\_L\_H is integrated in integrator 530a so as to obtain an indicator signal A\_L\_H.

15 The indicator signal is a measure for the deviation of the signals measured by sensors HFM\_1, HFM\_2; from this deviation it is possible to ~~conclude~~ determine the water quantity introduced in intake manifold 4. Differential signal Z\_Diff indicates which one of the two sensors HFM\_1, HFM\_2 detects a greater signal change.

20 As soon as indicator signal A\_L\_H exceeds a predefinable threshold value, controlled variable R (not shown in Figure 4) is obtained either from air-mass sensor signal L\_1 or from first auxiliary signal H\_1.

25 To obtain the most reliable value for the measured air mass for forming controlled variable R, the sensor signal whose signal change is smaller is used to form controlled variable R in this case.

30 If differential signal Z\_Diff > 0, the signal change of air-mass sensor signal L\_1 is greater than the signal change of first auxiliary signal H\_1; in this case, air-mass sensor signal L\_1 is ignored and controlled variable R is generated  
35 from first auxiliary signal H\_1. In an analogous manner, controlled variable R is formed from air-mass sensor signal

L\_1 in a negative differential signal Z\_Diff.

With the aid of indicator signal A\_L\_H from which the introduced water quantity may be ~~concluded~~ determined, and using the individual, not ignored sensor signal as a measure for the actual air quantity in intake tract 3, controlled variable R is able to be formed so as to calculate the correct fuel quantity to be injected as a function of the air mass actually available in the combustion chamber.

Both air-mass sensors HFM\_1, HFM\_2 may also be arranged next to one another in intake manifold 4, second air-mass sensor HFM\_2 being provided with a water separator (not shown). Since the water separator modifies the dynamic response of second air-mass sensor HFM\_2, a model of the dynamic response of the water-droplet separator ~~must be~~ is connected downstream from first air-mass sensor HFM\_1 in order to ensure comparability of the two sensor signals.

In this ~~variant~~ embodiment, a deviation of the sensor signals of both air-mass sensors HFM\_1, HFM\_2 provides a measure for the water quantity that has entered intake manifold 4. Both air-mass sensors HFM\_1, HFM\_2 ~~are preferably~~ may be arranged in the same housing.

## Summary

## ABSTRACT

~~The present invention relates to a~~ A method and a control unit  
for operating an internal combustion engine (1) of a motor  
5 vehicle are provided, in particular, ~~including a control unit~~  
(2) for controlling/regulating the internal combustion engine  
(1) as a function of an air-mass sensor signal (L<sub>1</sub>) from a  
first air-mass sensor ~~(HFM<sub>1</sub>)~~. A first auxiliary signal  
(H<sub>1</sub>), which is obtained arithmetically from an additional  
10 sensory system or ~~also~~ from models of the internal combustion  
engine (1), allows a plausibility control or ~~also~~ the  
substitution of the air-mass sensor signal (L<sub>1</sub>) in the case  
of signal interference of the air-mass sensor signal (L<sub>1</sub>),  
and thereby ensures that the internal combustion engine (1) is  
15 able to continue working in the optimal operating point.

~~(Figure 2)~~